

# INTERNATIONAL JOURNAL FOR ADVANCE RESEARCH IN ENGINEERING AND TECHNOLOGY

WINGS TO YOUR THOUGHTS.....

## ANALYSIS OF FBG PARAMETERS OF TANH PROFILE FOR DISPERSION COMPENSATION

Latika Chaudhary Pruthi<sup>1</sup>, Suraj Nagpal<sup>2</sup>

<sup>1</sup>M.Tech Scholar, <sup>2</sup>Assistant Professor

<sup>1</sup>GIMT Kanipla, <sup>2</sup>GIMT Kanipla

Kurukshetra, Pin no.136119

<sup>1</sup>latika1390@gmail.com, <sup>2</sup>nagpal.suraj@gmail.com

**Abstract:** Chirped fiber Bragg grating is a promising approach for dispersion compensation in optical fiber communication systems, since it is a passive optical component, fiber compatible, has low insertion losses and low cost. Many apodization profiles are suggested to optimize grating performance. Among them, hyperbolic tangent (tanh) apodization profile result in overall superior performance. In this work, the reflection spectrum of CFBG is evaluated by solving coupled mode equations and investigations have been done by varying various parameter for tanh apodization profile. Results show that, the characteristics of tanh apodized CFBG can be varied systematically according to effective apodization parameter ( $a_{eff}$ ) and apodization strength in the range 0.7-0.8. In optical communication CFBG can compensate linear dispersion of 100 km of standard optical fiber length, grating length 5 cm.

**Keywords:** Fiber bragg grating, dispersion compensation, chirped, apodization,

### 1. INTRODUCTION

The Optical fiber is one of the most important media in communication system [1]. Due to its several advantages and negligible transmission loss it is used in high speed data transmission [2-3].

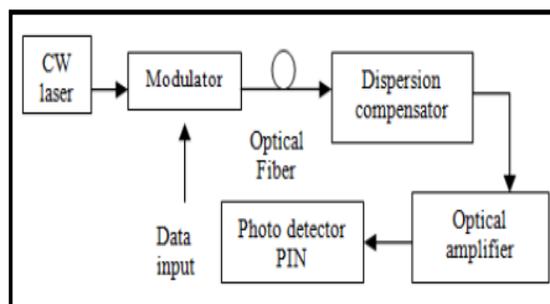


Figure 1: Optical communications block diagram

The main performance limiting factor in Optical Fiber Communication is the Dispersion [4]. In fiber optical high bit rate (such as 10Gb/s or 40Gb/s) long haul systems, dispersion compensation is the most important thing to be considered for design. Dispersion limits the bandwidth or information carrying capacity of a fiber[5]. Without dispersion compensation each symbol would be broadened and it would overlap with neighboring ones creating the distortion of the detected signal. [6].

There are many methods for dispersion compensation such as DCF, DSF, DFF, Chirped FBG, EDFA, Apodized FBG, Decision point adjustment etc. Comparisons have already been done to find that FBG is better than DCF [7]. DCF is also limited in optical input power to avoid nonlinear impairments, has a relatively high insertion loss and is bulky. Studies have also shown that pre compensation and post compensation methods have been realized based on FBG and DCF and it has been found that post compensation FBG performs better[8-9]

FBGs have negligible nonlinearity, low insertion loss and small size, all fiber configuration, highly selective filtering and flexibility. Their unique filtering properties and versatility as in-fiber devices are illustrated by their use in wavelength stabilized laser, fiber lasers, remotely pumped amplifiers, Raman amplifier, phase conjugators, converter, passive optical networks, wavelength division multiplexers/demultiplexers, add/drop multiplexer, gain equalizer and dispersion compensators. Two most important advances in FBG design are apodization and chirp. In chirped Fiber Bragg Grating (CFBG) the periodic variation of the refractive index is not constant which leads to different optical path length. Used as a dispersion compensator, the grating period could be reduced linearly down the length of grating (i.e. chirped mode). Therefore, the shorter wave-length is reflected at a point farther into the device than the longer wavelength. As intramodal dispersion reflects the fact that the shorter (blue) wavelength of the optical pulse travel faster than the longer (red) wavelength, this wavelength dependent time delay can be used to produce negative dispersion which is perfect to compensate dispersion in optical telecommunications system. CFBG fiber gratings show reflection spectra with large side lobes as well as highly nonlinear dispersion characteristics which are attributed to residual multiple reflections at the grating ends and can be significantly suppressed by a suitable variation (apodization) of the modulation depth along its length.[10] Unapodized CFBG fails to achieve the expected performance due to high ripples in time delay response. Various apodization profiles are suggested to optimize the grating performance and have been studied in literatures such as Gaussian, positive hyperbolic-tangent, quadratic-sine etc.[11] The dispersion is proportional to the length of the fiber. The length of optical fiber affects dispersion as increase in grating length leads to decrease in dispersion. When the length is increased the width becomes bulky and the magnitude reduces.[12] Various apodization profiles have been considered theoretically and experimentally in order to

# INTERNATIONAL JOURNAL FOR ADVANCE RESEARCH IN ENGINEERING AND TECHNOLOGY

WINGS TO YOUR THOUGHTS.....

smoothen the reflection spectrum and linearize the dispersion characteristics of aperiodic (chirped) gratings.[13] It has been realized that tight apodization profiles, in general, result in smooth features at the expense, however, of grating reflectivity, bandwidth, and dispersion. Excessively tight apodization profiles, on the other hand, might unnecessarily truncate gratings (reduce their effective length) and, in some applications, could impose severe limitations in the writing process. In this paper, hyperbolic tangent apodization profile is studied and analyzed systematically. The study is directed in term of bandwidth limitation and linearized time delay characteristics, which make CFBG suitable for use in dispersion compensation applications

## 2. LITERATURE REVIEW

Daniel paster et al investigated the equalization performance of various Apodization functions in linearly chirped fiber gratings with a view of determining an optimum profile for the design and fabrication of chromatic dispersion compensators Natalia M Litchinitser, Benjamin J. eggleton and David B. Patterson et al proposed a transmission based dispersion compensator employing an apodized unchirped fiber bragg grating and a figure of merit is defined for optimization of grating parameters for maximum recompression of dispersion broadened optical pulses in long-haul communication systems. The performance of transmission dispersion compensator can be improved by either making the grating longer or stronger.

Karin Ennsner, Michael N. Zervas and Richard I. Laming et al studied the dispersion characteristics of apodized, linearly chirped fiber bragg gratings and their potential as dispersion compensators. Positive hyperbolic tangent profile  $\tanh$  results in an overall superior performance as it provides highly linearized time delay characteristics with minimum reduction in linear dispersion. Jin Chai, Zhongyuan Yu, Yumin Liu et al 2006 present a system model that compensates dispersion of 100 km of standard single mode fiber and compares the effect of different Apodization sharpness on the spectral response.

Muhammed Faleh Hassan et al studied and analyzed the reflection spectrum and time delay characteristics of apodized linearly chirped fiber bragg grating. It is shown that truncation parameter of hyperbolic tangent Apodization profile plays an important role in optimizing chirped fiber bragg grating characteristics i.e. minimum reduction in FWHM reflection bandwidth and linearized time delay characteristics. There is an optimal performance at truncation parameter of 4 and bandwidth of 0.5 nm for 10 cm grating length over 100 km of standard fiber. Sher Shermin Azmiri Khan, Md. Saiful Islam et al 2011 investigated and compared the performances of various Apodization functions in linearly chirped apodized FBG. Six different Apodization profiles:  $\tanh$ , hamming, gauss, cos, Cauchy and sinc have been studied including their effects on the performances of dispersion compensator. It is demonstrated that Apodization profile is the key parameter for improving the spectral response which ultimately soothers the compensated dispersion in an optical transmission system

## 3. FIBER BRAGG GRATINGS

The principle of operation of FBG is Fresnel Reflection. It reflects a particular wavelength of light and transmits others. A fiber Bragg grating consists of a periodic modulation of the index of refraction along the core of an optical fiber. The fiber bragg grating is made so segments which reflects different wavelengths are in different positions along the length of fiber. Let the longer wavelengths arrived first and shorter wavelengths arrived last. The longer wavelengths are transmitted through to the last part of gratings and shorter wavelengths are reflected by the first part of grating. Due to this longer wavelength have to travel a longer distance, so they are delayed, allowing the shorter wavelength to catch up.[14] Layout of dispersion compensation module based on fiber bragg grating is shown below.

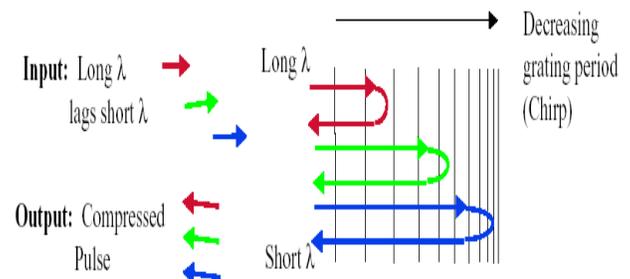


Figure 2: Principle of operation of FBG

Fiber Bragg Grating plays a significant role in optical fiber communication as filter, stabilizer, gain flattening filter, dispersion compensator, optical router etc.[15] Furthermore, it is also used as sensor for sensing temperature, pressure and strain etc. The FBG is a special form of optical fiber where the refractive index of the core is variable. As a result, the wavelength response of the fiber changes and various application emerge. The FBG is written inside the core of a photosensitive optical fiber using Ultraviolet rays[16,17]. The periodicity of FBG can be of two kinds. e.g mechanical like variation of the core diameter and optical like variation of the refractive index of the core. Two identical counter propagating modes, forward and backward, get coupled in FBG and the energy is transferred from the forward travelling to the backward travelling wave. As a result, we get reflection of the modal energy which is strongly wavelength dependency. The most noticeable feature of FBG is the flexibility of desired spectral characteristics. Numerous physical parameters can be varied including induced index change, length, apodization, period chirp, fringe tilt, and whether the grating supports counter propagating or co-propagating coupling at a desired wavelength. The parameter enable FBG to ensure the desired applications stated above. Wave propagation in optical fibers is analyzed by solving Maxwell's equations with appropriate boundary conditions. Many techniques are suggested for simulating fiber Bragg gratings [18]. All the techniques have varying degrees of complexity. However, the simplest method

# INTERNATIONAL JOURNAL FOR ADVANCE RESEARCH IN ENGINEERING AND TECHNOLOGY

*WINGS TO YOUR THOUGHTS.....*

is the straightforward numerical integration of the coupled-mode equations. In this contest, fiber Bragg Grating scattering of waves in a waveguide occurs when the refractive index is varying in the longitudinal direction. It can assume that the refractive index is varying as a quasi-sinusoidal function:

$$n(z) = n_0 + f(z) \cos\left[\left(\frac{2\pi}{\Lambda}\right)z + \theta(z)\right]$$

where,  $n_0$  is the fiber Bragg grating reference index,  $f(z)$  is the apodization function and  $\theta(z) = (2\pi/\Lambda)Cz^2$  is the chirping function where,  $C$  (in  $m^{-1}$ ) is the chirp parameter and  $\Lambda$  is the grating period. The functions  $f(z)$  and  $\theta(z)$  are slowly varying compared to  $\Lambda$ . If the fiber is in single mode operation, it supports only the fundamental mode, which has two components propagating in opposite directions. In the corrugated region, the forward propagating wave  $v_1$  and the backward propagating wave  $v_2$  are related by the coupled mode equations: [20]

$$\frac{dv_1(z; \delta)}{dz} = -i\delta v_1 + q(z)v_2$$

$$\frac{dv_2(z; \delta)}{dz} = +i\delta v_2 + q^*(z)v_1$$

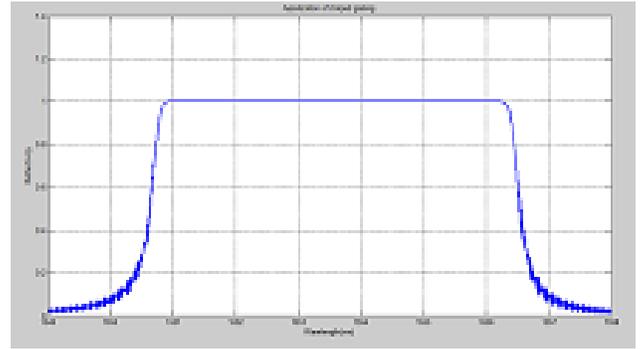
$v_1$  and  $v_2$  are the complex amplitude envelopes of the waves, obtained by removal of the spatial dependence  $\exp(\pm i\pi z/\Lambda)$ .  $q(z)$  is defined as the complex coupling coefficient  $q(z) = \frac{-i\pi}{2n_0\Lambda} f(z) \exp(-i\theta(z))$  and  $\delta$  is the phase shift per unit length compared to the Bragg wavelength  $\lambda_b = 2n_0\Lambda$ .

Fiber gratings are not infinite in length, so they have a beginning and an end. Thus, they begin abruptly and end abruptly. The Fourier transform of such a "rectangular" function immediately yields the well known *sinc* function, with its associated side-lobe structure apparent in the reflection spectrum. The transform of a Gaussian function, for example, is also a Gaussian, with no side lobes. A grating with a similar refractive modulation amplitude profile diminishes the side lobes substantially. The suppression of the side lobes in the reflection spectrum by gradually increasing the coupling coefficient with penetration into, as well as gradually decreasing on exiting from the grating, is called apodization.

Many apodization profiles have been suggested to optimize CFBG characteristics, such as raised sine, sine, sinc, tanh and Blackman profiles [19]. Study has been done on the effect of these profiles on the chirped fiber grating characteristics, and the optimum relation between the degree of the apodization and the resulting interrelated grating characteristic. Their results show that the hyperbolic-tangent apodization profile results in overall superior performance, as it provide dispersion compensators with highly linearized time delay characteristic with minimum reduction in linear dispersion, compared with the unapodized case.[20] The hyperbolic tangent profiles can be implemented using the following equation.

$$f(z) = \begin{cases} \tanh(a_{tr} z/L) & 0 \leq z \leq L/2 \\ \tanh(a_{tr} (L-z)/L) & L/2 \leq z \leq L \end{cases}$$

Where, the parameter  $a_{tr}$  is best to be called as truncation parameter, since it controls the truncation of the apodization function and,  $L$  is the CFBG length.[21]



**Figure 3:** Reflection Spectrum of Tanh profile

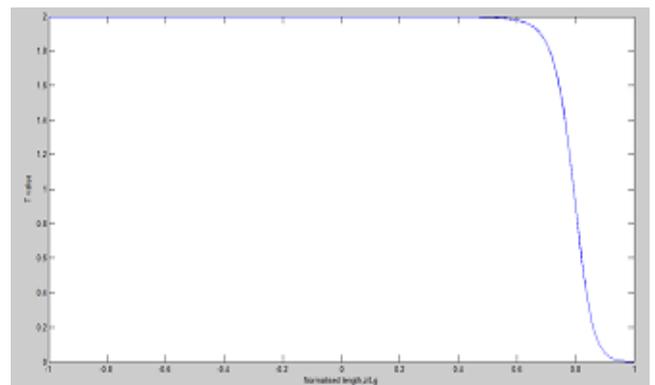
We define another parameter which is useful in our discussion is the apodization parameter  $a_{eff}$  [22]:

$$a_{eff} = \frac{\text{area of apodized FBG}}{\text{area of unapodized FBG}} = \frac{\int_0^L f(z) dz}{\int_0^L dz}$$

As shown in the figure, the reflectivity response of the tanh apodization profile shows maximum amplitude as unity

## 4. NEW PROPOSED SCHEME

The basic simulation parameter and simulation results are discussed in this section. Simulation study has been done by using MATLAB. Following the above mathematical formulation, we have plotted the optimization process for dispersion compensation. We divided grating length  $L_g$  into 200 small segments, Length of 1st period is  $l = 1.6\text{mm}$ , and linearly decrease by a factor of 0.99 mm thus we find that the gating length  $L_g = 5\text{cm}$ . After choosing the profile, we have investigated the spectral characteristics of the fiber bragg grating.



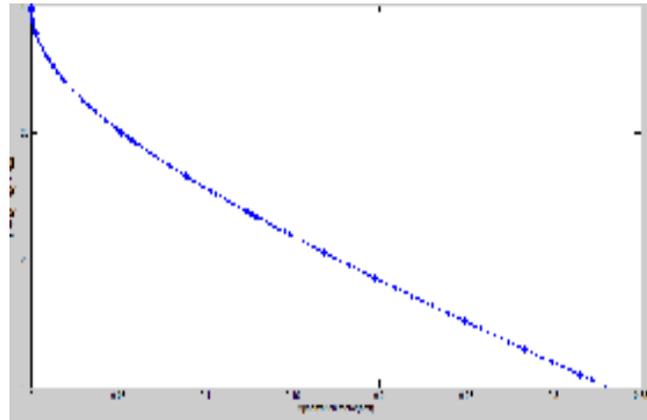
**Figure 4:** Variation of apodization profile tanh function with normalized length

# INTERNATIONAL JOURNAL FOR ADVANCE RESEARCH IN ENGINEERING AND TECHNOLOGY

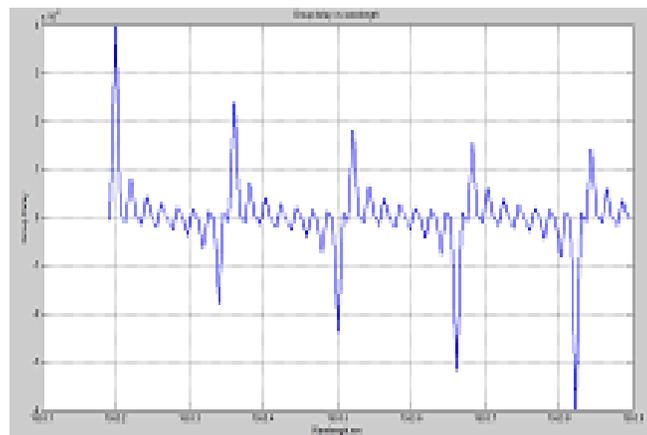
WINGS TO YOUR THOUGHTS.....

The hyperbolic tangent function is given by equation  $T(z)=1+\tanh[T\{1-2(\frac{z}{Lg})^\alpha\}]$

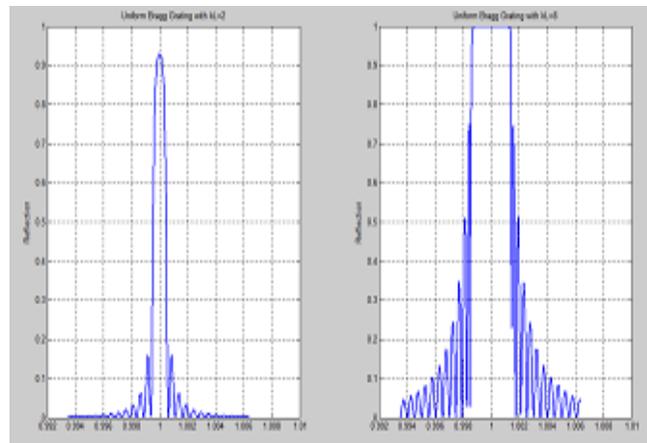
For this purpose we evaluated its reflectivity, apodization factor, group delay, grating strength, grating period and dispersion.



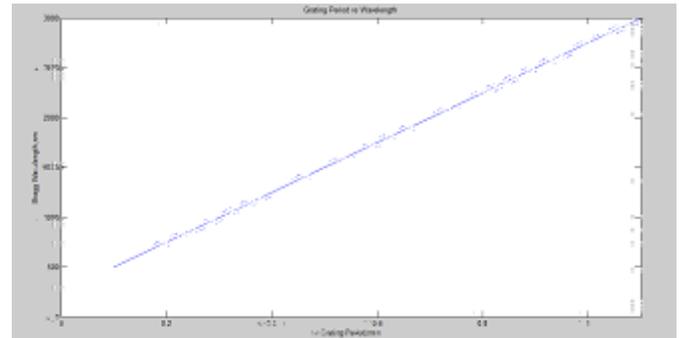
**Figure 5:** Grating length against apodization parameter



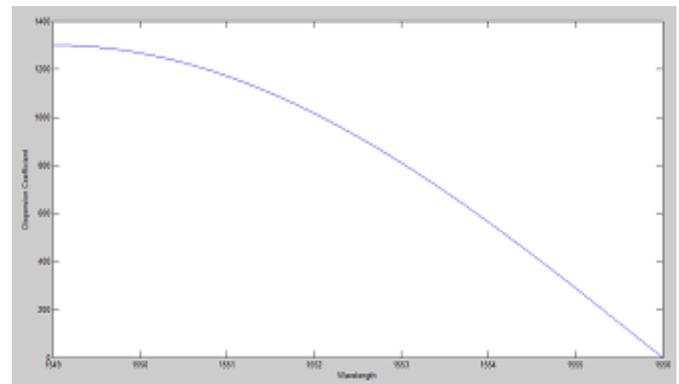
**Figure 6:** Group delay ripple response of tanh profile



**Figure 7:** Reflection spectra versus normalized wavelength for bragg grating with  $kL=2$  and  $kL=8$



**Figure 8:** Linearly chirped grating period versus Bragg wavelength



**Figure 9:** Dispersion coefficient versus wavelength using apodized FBG

## 5. CONCLUSIONS AND FUTURE WORK

In this paper, we investigated the variation of different FBG parameters on tanh apodization profile. We have found that the smaller the apodization parameter, the tighter the apodization profile. Small apodization parameters correspond to small grating effective lengths. For unapodized gratings,  $a_{eff}=1$ . In the figure it is evident that the apodization function of the tanh apodization profile with  $\alpha=4, \beta=4$  has maximum amplitude equals to 2. Also, the value of apodization factor comes out to be 0.7 for the minimum grating length of 5cm as seen in figure 4. The group delay ripple gives maximum peak value at  $3.977e-008$  at 1553 nm and minimum peak value at  $-3.99e-008$  at 1554 nm. The strength of the grating evaluated for  $kL=2$  and  $kL=8$  as shown in figure 6 and also it gives more side lobes for  $kL=8$ . The graph plotted between grating period and bragg wavelength shows that the grating period increases with the increase in wavelength and min wavelength of 500 nm at grating period 0.1. In our future work, we work on the improving the value of dispersion for minimum length of gratings and for multimode fiber.

## References

- [1] Natalia M. Litchinitser , Benjamin J. Eggleton, and David B. Patterson, "Fiber Bragg Grating for Dispersion Compensation in Transmission: Theoretical Model and

# INTERNATIONAL JOURNAL FOR ADVANCE RESEARCH IN ENGINEERING AND TECHNOLOGY

WINGS TO YOUR THOUGHTS.....

Design Criteria For Nearly Ideal Pulse Recompression”, journal of lightwave technology vol 15 No. 8, August 1997.

[2] M.A Othman, M.M Ismail, H.A Sulaiman, M.H Misran, M.A Meor Said, Y.A Rahim, A.N Che Pee, M.R Motsidi, “An Analysis of 10Gbits/s Optical Transmission System using fiber Bragg Grating, IOSRJEN, vol 2, issue 7, pp 55-61, 2012.

[3] Johannes Skaar, "Synthesis and characterization of fiber Bragg Gratings”, November, 7, 2000.

[4] Er. Abhishek Sharma, Er Sukhbir Singh, Er. Bhubneshwar Sharma, “Investigations on dispersion compensation using fiber braggs grating”, IJCA , vol 73, no 2, 2013.

[5] Ojuswini Arora, Amit Kumar Garg, “Dispersion Compensation for High Speed Optical Networks”, IJECE, vol 2, pp1-4, 2012

[6] Ojuswini Arora, Amit Kumar Garg, “Dispersion Compensation for High Speed Optical Networks”, IJECE, vol 2, pp1-4, 2012.

[7] Gnanam Gnanagurunathan, Faidz Abd. Rahman, ‘Comparing FBG and DCF as dispersion compensators in the long haul narrowband wdm systems”, IEEE 2006.

[8] Manjit Singh, Ajay K. Sharma, R.S Kaler, “Investigations on order and width of RZ super gaussian pulse in pre-, post- and symmetrical dispersion compensated 10gb/s optical communication system using standard and dispersion compensating fibers”, optics 121 pp 609-616 elsevier journal 2008.

[9] K. Khairi, Z. Lambak, Norhakimah Md Samsuri, Z. Hamzah, Fong Kok Hann, “Investigation on the performance of pre and post compensation using multi channel CFBG dispersion compensators”, International RF and Microwave conference IEEE 2011.

[10] D. Pastor, J. Capmany, D. Ortega, V. Tatay, and J. Marti, “Design of apodized linearly chirped fiber gratings for dispersion compensation,”*J. Lightwave Technol.*, vol. 14, pp. 2581–2588, Nov. 1996.

[11] Karin Ennser, Mikhail N. Zervas, and Richard I. Laming, " Optimization of Apodized Linearly Chirped Fiber Gratings for Optical Communications", IEEE Journal of Quantum electronic, VOL. 34, NO. 5, pp.770-778, MAY 1998.

[12] Md. Jahidul Islam, Md. Saiful Islam, Md. Mahmudur Rahman,, “Dispersion compensation in optical fiber communication using fiber bragg grating”, 2012.

[13] M. N. Zervas, K. Ennser, and R. I. Laming, “Design of apodized linearly- chirped fiber gratings for optical communications,” in Proc. 22nd Eur. Conf. Optical Communications (ECOC 96), Oslo, Norway, 1996, vol. 3, pp. 233– 236.

[14] S. O. Mohammadi, Saeed Mozaffari and M. Mahdi Shahidi, “Simulation of a transmission system to compensate dispersion in an optical fiber by chirp gratings’, international journal of the physical sciences vol. 6, no. 32, pp. 7354-7360, 2011.

[15] Devendra Kr. Tripathi, Pallavi Singh, N.K Shukla, H.K Dixit, “Performance study in dispersion compensation techniques with duo binary format at different bit rates”, ICPCES, IEEE 2012.

[16] Wen liu, shu-qin guo, li-ping chang, ming lei, fu-mei sun, “The research on 10gbps optical communication dispersion compensation systems without electric regenerator”, 3<sup>rd</sup> international congress on image and signal processing, IEEE 2010.

[17] Md. Jahidul Islam, Md. Saiful Islam, Md. Mahmudur Rahman, “Dispersion compensation in optical fiber communication using fiber bragg grating”, Global Journal Of Researches In Engineering Electrical and Electronics Engineering, Vol 12, issue 2, 2012.

[18] Smita S. Dabhade, Savita Bhosale, ‘Fiber Bragg Grating and Phase Conjugator As Dispersion Compensator”, International Journal on Advanced Electrical and Electronics Engineering, (IJAEED), Vol. 1, Issue 1, pp. 15-19, 2012.

[19] Naqib Muhammad Faiyaz, Asif Iftekhar Omi, Mohammad Faisal, “Optimization of apodization profile of chirped fiber bragg grating for chromatic dispersion compensation”, ICEEICT, IEEE 2014.

[20] Karin Ennser, Mikhail N. Zervas, and Richard I. Laming, " Optimization of Apodized Linearly Chirped Fiber Gratings for Optical Communications", IEEE Journal of Quantum electronic, Vol. 34, No. 5, pp.770-778, May 1998.

[21] Sher Shermin Azmiri Khan, Md. Saiful Islam, “Performance evaluation of different apodization profiles of linearly chirped fbg for dispersion compensation”, ICCIT, IEEE 2011.

[22] P. S. Cross and H. Kolgenik, “Sidelobe suppression in corrugated waveguide filters,” *Opt. Lett.*, vol. 1, pp. 43–45, 1977.